Title

KINEMATICS OF MACHINES

Sub-title

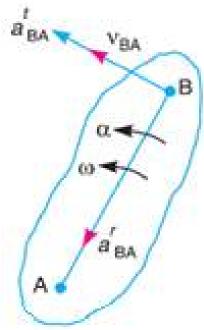
Velocity & Acceleration Analysis

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Acceleration in Mechanisms

Acceleration of a particle whose velocity changes both in magnitude and direction at any instant has the following two components:

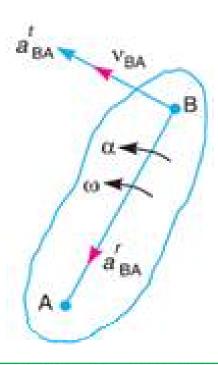
- The centripetal or radial component, which is perpendicular to the velocity of the particle at the given instant.
- The tangential component, which is parallel to the velocity of the particle at the given instant.



$$a_{\rm BA}^r = \omega^2 \times \text{Length of link } AB$$

$$= \omega^2 \times AB = v_{BA}^2 / AB \qquad \dots \left(: \omega = \frac{v_{BA}}{AB} \right)$$

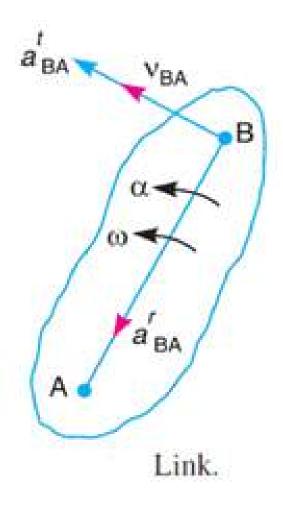
This radial component of acceleration acts perpendicular to the velocity $v_{\rm BA}$, In other words, it acts *parallel to the link AB*.

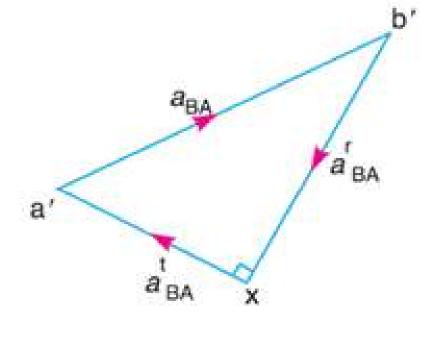


We know that tangential component of the acceleration of B with respect to A,

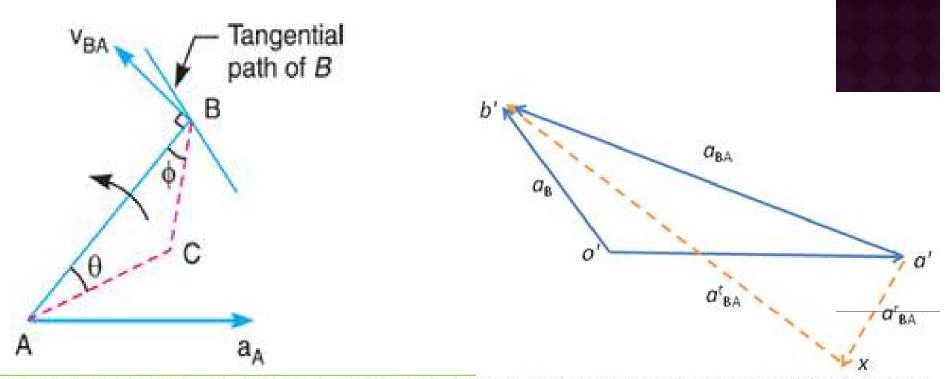
$$a_{\rm BA}^t = \alpha \times \text{Length of the link } AB = \alpha \times AB = \frac{\text{dv}}{\text{dt}}$$

This tangential component of acceleration acts parallel to the velocity v_{BA} . In other words, it acts *perpendicular* to the link AB.





Acceleration of a Point on a Link

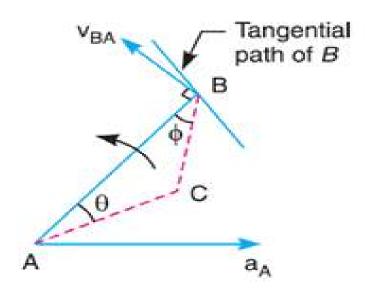


From any point o', draw vector o'a' parallel to the direction of absolute acceleration at point A i.e. a_A , to some suitable scale

Draw vector a'x parallel to the link AB (because radial component of the acceleration of B with respect to A will pass through AB), such that

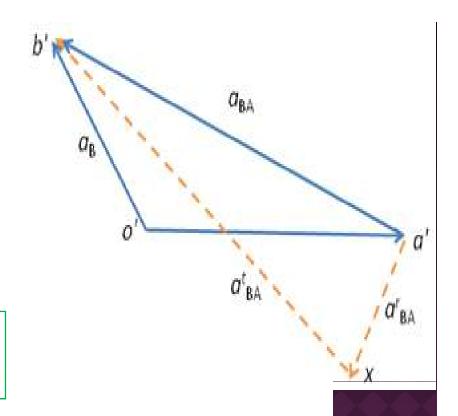
vector
$$a'x = a_{BA}^r = v_{BA}^2 / AB$$

where v_{BA} = Velocity of B with respect to A.



From point x, draw vector xb' perpendicular to AB or vector a'x i.e. a'_{RA}

through o' draw a line parallel to the path of B to represent the absolute acceleration of B i.e. a_B . The vectors xb' and o'b' intersect at b'. Now the values of a_B and a'_{BA} may be measured, to the scale.



$$\alpha_{AB} = a_{BA}^t / AB$$

By joining the points a' and b' we may determine the total acceleration of B with respect to A i.e. a_{BA} . The vector a' b' is known as acceleration image of the link AB.

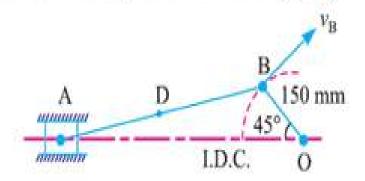
Example 8.1. The crank of a slider crank mechanism rotates clockwise at a constant speed of 300 r.p.m. The crank is 150 mm and the connecting rod is 600 mm long. Determine: 1. linear velocity and acceleration of the midpoint of the connecting rod, and 2. angular velocity and angular acceleration of the connecting rod, at a crank angle of 45° from inner dead centre position.

Solution. Given: $N_{BO} = 300$ r.p.m. or $\omega_{BO} = 2 \pi \times 300/60 = 31.42$ rad/s; OB = 150 mm = 0.15 m; BA = 600 mm = 0.6 m

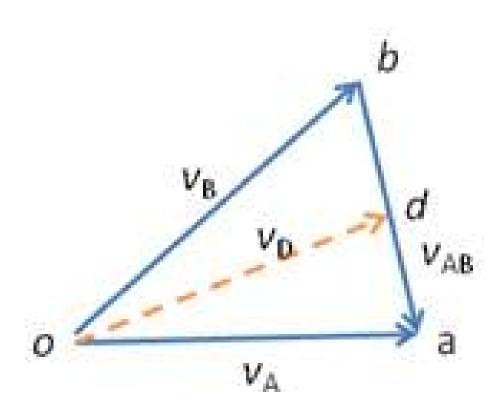
We know that linear velocity of B with respect to O or velocity of B,

$$v_{\text{BO}} = v_{\text{B}} = \omega_{\text{BO}} \times OB = 31.42 \times 0.15 = 4.713 \text{ m/s}$$

1. First of all draw the space diagram, to some suitable scale; as shown in Fig. (a).



(a) Space diagram.



Acceleration of the midpoint of the connecting rod

• We know that the radial component of the acceleration of B with respect to O or the acceleration of B, $a'_{BO} = a_{B} = \frac{v_{BO}^{2}}{O B} = \frac{(4.713)^{2}}{O 15} = 148.1 \text{ m/s}^{2}$

and the radial component of the acceleration of A with respect to B,

$$a_{AB}^r = \frac{v_{AB}^2}{BA} = \frac{(3.4)^2}{0.6} = 19.3 \text{ m/s}^2$$

- NOTE:1) A point at the end of a link which moves with constant angular velocity has no tangential component of acceleration.
 - When a point moves along a straight line, it has no centripetal or radial component of the acceleration.

(a) Space diagram.

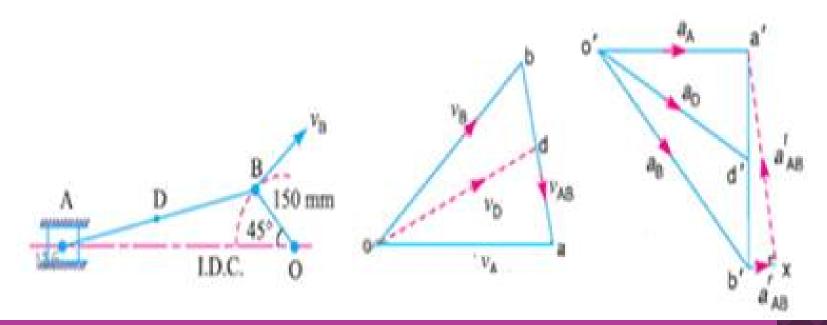
(b) Velocity diagram.

Acceleration of the midpoint of the connecting rod

Draw vector o'b' parallel to BO, to some suitable scale,

vector
$$a'b' = a'_{BO} = a_B = 148.1 \text{ m/s}^2$$

Note: Since the crank *OB* rotates at a constant speed, therefore there will be no tangential component of the acceleration of *B* with respect to *O*.



from point b', draw vector b' x parallel to AB to represent $a'_{AB} = 19.3 \text{ m/s}^2$ and from point x draw vector xa' perpendicular to vector b' x whose magnitude is yet unknown.

Now from o', draw vector o'a' parallel to the path of motion of A (which is along AO) to represent the acceleration of A i.e. a_A . The vectors xa' and o'a' intersect at a'. Join a'b'.

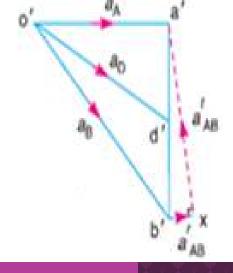
In order to find the acceleration of the midpoint D of the connecting rod A B, divide the vector a' b' at d' in the same ratio as D divides A B. In other words

$$b'd'/b'a' = BD/BA$$

Join o'd'. The vector o'd' represents the acceleration of midpoint D of the connecting rod

By measurement, we find that

$$a_D$$
 = vector o' d' = 117 m/s² Ans.



Angular velocuy of the connecting roa

We know that angular velocity of the connecting rod AB,

$$\omega_{AB} = \frac{v_{AB}}{BA} = \frac{3.4}{0.6} = 5.67 \text{ rad/s}$$
Ans.

Angular acceleration of the connecting rod

From the acceleration diagram, we find that

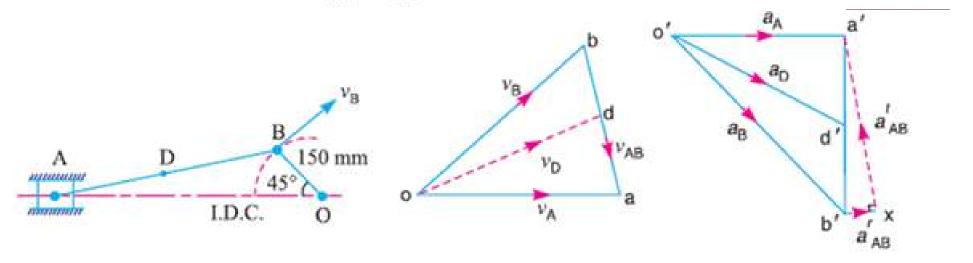
$$a_{AB}^{t} = 103 \text{ m/s}^2$$

...(By measurement)

We know that angular acceleration of the connecting rod AB,

$$\alpha_{AB} = \frac{a'_{AB}}{BA} = \frac{103}{0.6} = 171.67 \text{ rad/s}^2$$

Ans.



(a) Space diagram.

- (b) Velocity diagram.
- (c) Acceleration diagram.

Example 8.4. PORS is a four bar chain with link PS fixed. The lengths of the links are PQ = 62.5 mm; QR = 175 mm; RS = 112.5 mm; and PS = 200 mm. The crank PQ rotates at 10 rad/s clockwise. Draw the velocity and acceleration diagram when angle QPS = 60° and Q and R lie on the same side of PS. Find the angular velocity and angular acceleration of links QR and RS.

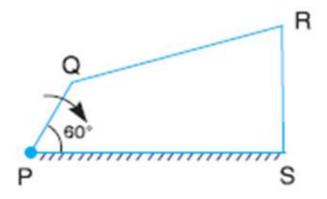
Solution. Given: $\omega_{OP} = 10 \text{ rad/s}$; PQ = 62.5 mm = 0.0625 m; QR = 175 mm = 0.175 m; RS = 112.5 mm = 0.1125 m; PS = 200 mm = 0.2 m

We know that velocity of Q with respect to P or velocity of Q,

$$v_{\rm OP} = v_{\rm O} = \omega_{\rm OP} \times PQ = 10 \times 0.0625 = 0.625 \text{ m/s}$$

Angular velocity of links QR and RS

First of all, draw the space diagram of a four bar chain, to some suitable scale



(a) Space diagram.

1. Since P and S are fixed points, therefore these points lie at one place in velocity diagram. Draw vector pq perpendicular to PQ, to some suitable scale, to represent the velocity of Q with respect to P or velocity of Q i.e. v_{OP} or v_{O} such that

vector
$$pq = v_{OP} = v_{O} = 0.625 \text{ m/s}$$

2. From point q, draw vector qr perpendicular to QR to represent the velocity of R with respect to $Q(i.e.\ v_{RQ})$ and from point s, draw vector sr perpendicular to SR to represent the velocity of R with respect to S or velocity of R ($i.e.\ v_{RS}$ or v_{R}). The vectors qr and sr intersect at r. By measurement, we find that

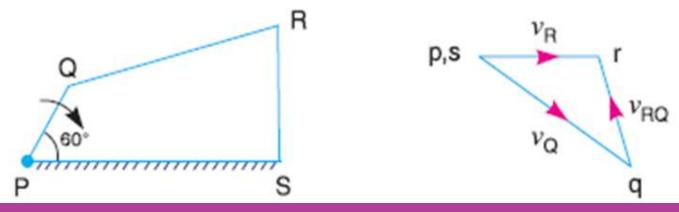
$$v_{RQ}$$
 = vector $qr = 0.333$ m/s, and $v_{RS} = v_R$ = vector $sr = 0.426$ m/s

We know that angular velocity of link QR,

$$\omega_{QR} = \frac{v_{RQ}}{RQ} = \frac{0.333}{0.175} = 1.9 \text{ rad/s (Anticlockwise) Ans.}$$

and angular velocity of link RS,

$$\omega_{RS} = \frac{v_{RS}}{SR} = \frac{0.426}{0.1125} = 3.78 \text{ rad/s (Clockwise)}$$
 Ans.



Angular acceleration of links OR and RS

Since the angular acceleration of the crank PQ is not given, therefore there will be no tangential component of the acceleration of Q with respect to P.

We know that radial component of the acceleration of Q with respect to P (or the acceleration of Q).

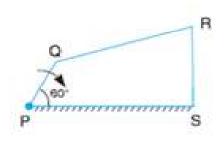
$$a_{\text{QP}}^r = a_{\text{QP}} = a_{\text{Q}} = \frac{v_{\text{QP}}^2}{PQ} = \frac{(0.625)^2}{0.0625} = 6.25 \text{ m/s}^2$$

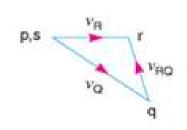
Radial component of the acceleration of R with respect to Q,

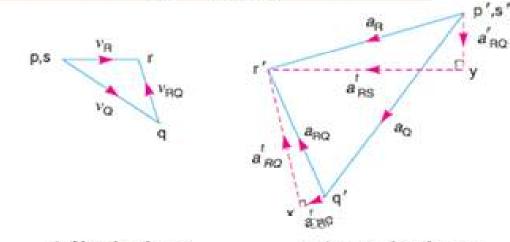
$$a_{\text{RQ}}^r = \frac{v_{\text{RQ}}^2}{QR} = \frac{(0.333)^2}{0.175} = 0.634 \text{ m/s}^2$$

and radial component of the acceleration of R with respect to S (or the acceleration of R),

$$a_{RS}^r = a_{RS} = a_R = \frac{v_{RS}^2}{SR} = \frac{(0.426)^2}{0.1125} = 1.613 \text{ m/s}^2$$



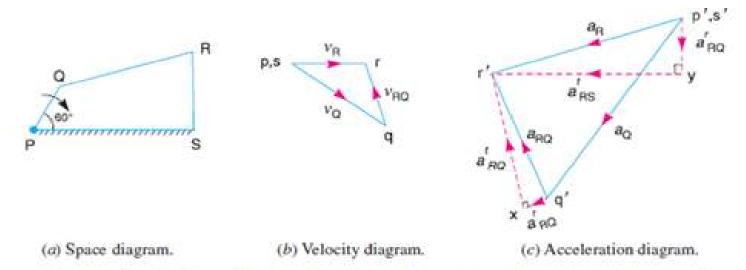




(a) Space diagram.

(b) Velocity diagram.

(c) Acceleration diagram.



1. Since P and S are fixed points, therefore these points lie at one place in the acceleration diagram. Draw vector p'q' parallel to PQ, to some suitable scale, to represent the radial component of acceleration of Q with respect to P or acceleration of Q i.e a'_{QP} or a_{Q} such that

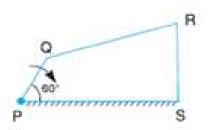
vector
$$p'q' = a_{OP}' = a_{O} = 6.25 \text{ m/s}^2$$

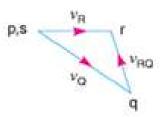
2. From point q', draw vector q' x parallel to QR to represent the radial component of acceleration of R with respect to Q i.e. a_{RO}^r such that

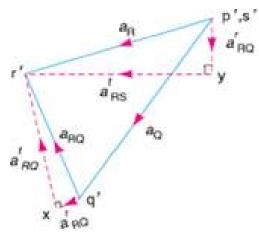
vector
$$q'x = a_{RQ}^r = 0.634 \text{ m/s}^2$$

- 3. From point x, draw vector xr' perpendicular to QR to represent the tangential component of acceleration of R with respect to Qi.e a_{RO}^{i} whose magnitude is not yet known.
- 4. Now from point s', draw vector s'y parallel to SR to represent the radial component of the acceleration of R with respect to S i.e. a_{RS}^r such that

vector
$$s'y = a_{RS}^r = 1.613 \text{ m/s}^2$$







(a) Space diagram.

(b) Velocity diagram.

(c) Acceleration diagram.

- 5. From point y, draw vector yr' perpendicular to SR to represent the tangential component of acceleration of R with respect to Si.e. a_{RS}^{I} .
 - 6. The vectors xr' and yr' intersect at r'. Join p'r and q'r'. By measurement, we find that $a'_{RQ} = \operatorname{vector} xr' = 4.1 \text{ m/s}^2$ and $a'_{RS} = \operatorname{vector} yr' = 5.3 \text{ m/s}^2$

We know that angular acceleration of link QR,

$$\alpha_{QR} = \frac{a'_{RQ}}{QR} = \frac{4.1}{0.175} = 23.43 \text{ rad/s}^2 \text{ (Anticlockwise) Ans.}$$

and angular acceleration of link RS,

$$\alpha_{RS} = \frac{a'_{RS}}{SR} = \frac{5.3}{0.1125}$$
 Anticlockwise Ans.

Angular acceleration of links QR and RS

Since the angular acceleration of the crank PQ is not given, therefore there will be no tangential component of the acceleration of Q with respect to P.

We know that radial component of the acceleration of Q with respect to P (or the acceleration of Q),

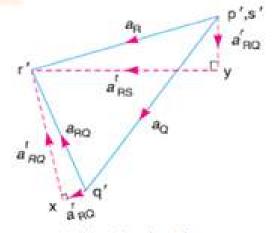
$$a_{\text{QP}}^{r} = a_{\text{QP}} = a_{\text{Q}} = \frac{v_{\text{QP}}^{2}}{PQ} = \frac{(0.625)^{2}}{0.0625} = 6.25 \text{ m/s}^{2}$$

Radial component of the acceleration of R with respect to Q,

$$a_{\text{RQ}}^r = \frac{v_{\text{RQ}}^2}{QR} = \frac{(0.333)^2}{0.175} = 0.634 \text{ m/s}^2$$

and radial component of the acceleration of R with respect to S (or the acceleration of R),

$$a_{RS}^r = a_{RS} = a_R = \frac{v_{RS}^2}{SR} = \frac{(0.426)^2}{0.1125} = 1.613 \text{ m/s}^2$$



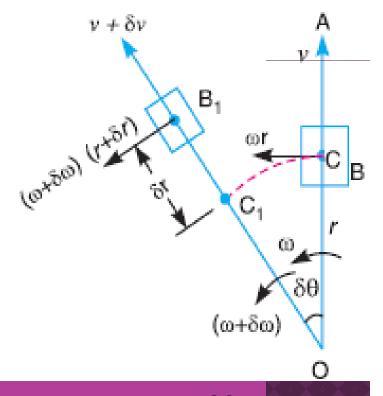
(c) Acceleration diagram.

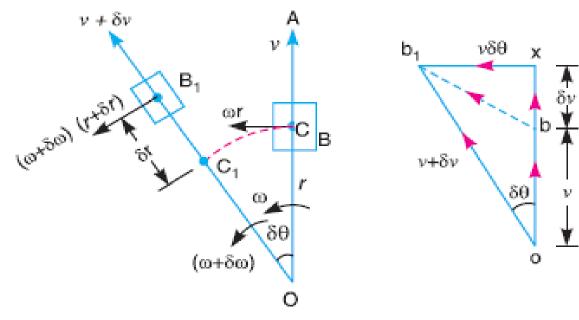
Coriolis Component of Acceleration

When a point on one link is sliding along another rotating link, such as in quick return motion mechanism, then the coriolis component of the acceleration must be calculated.

Consider a link OA and a slider B as shown in Fig. link OA. The point C is the coincident point on the link OA.

The slider B moves along the





$$bx = ox - ob = (v + \delta v) \cos \delta \theta - v \uparrow$$

Since $\delta\theta$ is very small, therefore substituting $\cos\delta\theta=1$, we have

$$bx = (v + \delta v - v) \uparrow = \delta v \uparrow$$

...(Acting radially outwards)

and

$$xb_1 = (v + \delta v) \sin \delta \theta$$

Since $\delta\theta$ is very small, therefore substituting $\sin\delta\theta=\delta\theta$, we have

$$xb_1 = (v + \delta v) \delta\theta = v.\delta\theta + \delta v.\delta\theta$$

Neglecting $\delta v.\delta \theta$ being very small, therefore

$$xb_1 = v. \overleftarrow{\delta \theta}$$

Fig. shows the velocity diagram when the velocities ωr and $(\omega + \delta \omega) (r + \delta r)$ are considered.

$$yb_1 = (\omega + \delta\omega) (r + \delta r) \sin \delta\theta \downarrow$$

= $(\omega r + \omega \delta r + \delta\omega r + \delta\omega \delta r) \sin \delta\theta$

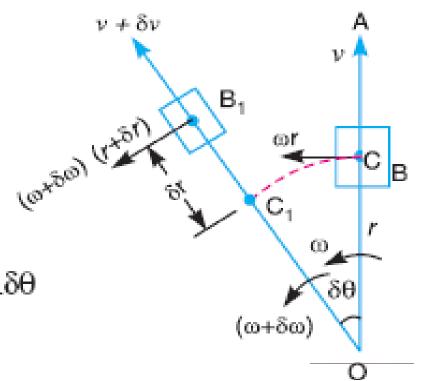
$$yb_1 = \omega .r.\delta\theta + \omega .\delta r.\delta\theta + \delta\omega .r.\delta\theta + \delta\omega .\delta r.\delta\theta$$

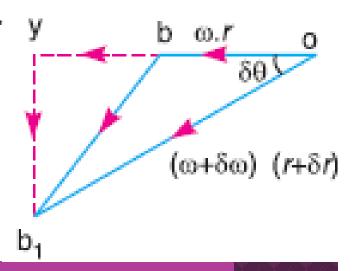
= $\omega .r.\delta\theta \downarrow$, acting radially inwards

$$by = oy - ob = (\omega + \delta\omega) (r + \delta r) \cos \delta\theta - \omega r$$
$$= (\omega r + \omega \delta r + \delta\omega r + \delta\omega \delta r) \cos \delta\theta - \omega r$$

 $by = \omega . r + \omega . \delta r + \delta \omega . r + \delta \omega . \delta r - \omega . r = \omega . \delta r + r . \delta \omega$ total component of change of velocity along radial direction

$$= bx - yb_1 = (\delta v - \omega r . \delta \theta) \uparrow$$





 \therefore Radial component of the acceleration of the slider B with respect to O on the link OA,

$$a_{\rm BO}^r = \operatorname{Lt} \frac{\delta v - \omega r \cdot \delta \theta}{\delta t} = \frac{dv}{dt} - \omega r \times \frac{d\theta}{dt} = \frac{dv}{dt} - \omega^2 r \uparrow$$
 (: $d\theta/dt = \omega$)

total component of change of velocity along tangential direction,

$$=xb_1+by=v.\delta\theta+(\omega.\delta r+r.\delta\omega)$$
 (Perpendicular to OA and towards left)

Tangential component of acceleration of the slider B acting perpendicular to OA and towards left,

$$a_{\text{BO}}^{t} = \text{Lt} \frac{v.\delta\theta + (\omega.\delta r + r.\delta\omega)}{\delta t} = v \frac{d\theta}{dt} + \omega \frac{dr}{dt} + r \frac{d\omega}{dt}$$

$$= v.\omega + \omega.v + r.\alpha = (2v.\omega + r.\alpha) \qquad (\because dr/dt = v, \text{ and } d\omega/dt = \alpha)$$

$$a_{BO}^{r} = \frac{dv}{dt} - \omega^{2} .r \uparrow$$

$$a_{BO}^{t} = (2v.\omega + r.\alpha)$$

$$a_{CO}^r = \omega^2 r \uparrow$$

$$a_{CO}^t = \overset{\leftarrow}{\alpha}.r \uparrow$$

$$a_{\mathrm{BC}}^{r} = a_{\mathrm{BO}}^{r} - a_{\mathrm{CO}}^{r} = \left(\frac{dv}{dt} - \omega^{2} r\right) - \left(-\omega^{2} r\right) = \frac{dv}{dt} \uparrow$$

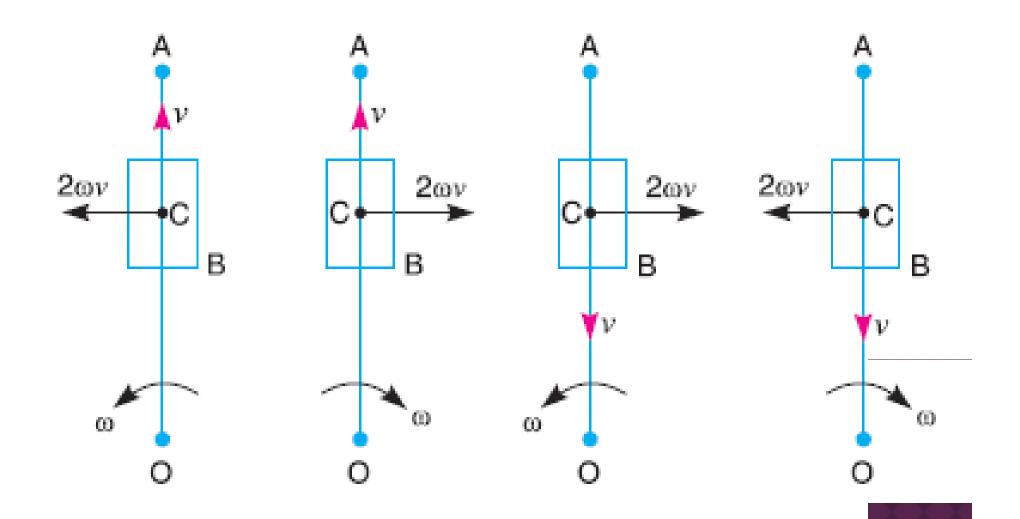
$$a_{\mathrm{BC}}^{t} = a_{\mathrm{BO}}^{t} - a_{\mathrm{CO}}^{t} = (2 \omega v + \alpha r) - \alpha r = 2 \omega v$$

Coriolis component of the acceleration of B with respect of C,

$$a_{BC}^c = a_{BC}^t = 2 \omega v$$

 ω = Angular velocity of the link OA, and

v = Velocity of slider B with respect to coincident point C.



Direction of coriolis component of acceleration.

Thank You